RESEARCH ARTICLE

Magnetic Field Sensing by Magnetic-Fluid-Coated Capillary Long-Period Fiber Gratings





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Abstract: In this paper, we presented and experimentally investigated a novel magnetic field sensor (MFS) based on magnetic fluid (MF)-coated capillary long-period fiber gratings (CLPFGs). The CLPFGs with short length of no more than 10 mm and period of 1 mm were fabricated by point-to-point arc discharge method and then infiltrated in an MF-filled glass tube forming a packaged MF-coated CLPFGs MFSs. A redshift in resonances of CLPFGs was brought out after packaging process, due to external refractive index changing. With the increasing external magnetic field, the intensity of resonant dips gradually decreased, which is caused by magnetostrictive effect together with refractive index variations. Moreover, CLPFGs with the same grating period and different grating lengths were comparatively investigated and analyzed. The resonant dips with larger transmissive depth present faster descend to the external magnetic field, resulting in higher sensitivity. The sensitivity of 0.036 dB/Oe could be obtained, when the CLPFGs have a grating length of 9 mm. What is more, the sensor is insensitive to temperature, which can avoid the effect of temperature. The proposed MF-coated CLPFGs MFS has potential applications in magnetic field systems.

Keywords: long-period fiber grating, optical fiber sensing, magnetic field sensor, magnetic fluid

1. Introduction

Recently, magnetic field sensor (MFS) has played an increasingly important role in biomedical testing, aerospace industry space, and geophysical research [1-3]. The conventional electric MFSs are mostly based on the sensing principles such as Hall effect [4], magnetoresistive effect [5], and fluxgate [6]. Fiberoptic MFSs outperform the electric MFSs, because it is light in weight, small in size, low in cost, and can be remotely controlled. Nowadays, fiber-optic MFSs are mainly based on Faraday effect [7] and magnetostrictive materials [8]. However, it is difficult to integrate magnetostrictive materials with optical fibers in some cases. At present, fiber-optic MFSs based on magneto-opticaleffect have drawn increasing amounts of attention, among which magnetic fluid (MF) has been widely used as a sensitive component for magnetic field detection. The MF-based fiber-optic MFSs have good temperature stability and optical stability, which can maintain stable performance over a wide temperature range and is not easily affected by external interference. Moreover, the sensing element of the MF-based fiber-optic MFSs is composed of MF and optical fiber, without mechanical components, so it has a long lifespan.

Different types of MF-based fiber-optic MFSs have been proposed, such as grating-based sensors including fiber Bragg

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grating (FBG) [9], tilted FBG [10], long-period fiber gratings (LPFGs) [11], and interferometric sensors such as Fabry-Perot interferometer (FPI) [12], Mach-Zehnder interferometer (MZI) [13], Michelson interferometer [14], and Sagnac interferometer [15]. Hollow core fiber (HCF), due to large refractive index difference between the cladding and hollow core, has been developed in magnetic field sensing fields. By utilizing the magneto-volume effect, the magnetic field sensitivity of FPI-based MFS is greatly improved [16]. Using the U-shaped HCF, simultaneous measurement of magnetic field and temperature could be achieved [17]. An MZI-based MFS is formed, with interference between the LP₀₁ and LP₁₁ modes in HCF, which can achieve a higher sensitivity [18]. Moreover, magnetic field sensing measurement could be realized by connecting the corroded HCF to the taper fiber, which produces a whispering gallery mode resonance spectrum [19]. Apart from the above structures, the grating-based MFSs have also aroused great interest. Using the tapered FBG, the MFS can achieve intensitymodulated and large bandwidth measurement [20]. A vector MFS can be achieved by sealing the eccentric FBG into an MF-infiltrated glass capillary [21]. LPFGs have the advantages of the simplicity of configuration measurement and higher sensitivity. Based on MF-coated LPFGs within a standard singlemode fiber (SMF), the transmission minimum of the MFS is highly sensitive to the change of ambient medium [22]. The dispersion turning point-based LPFGs can achieve a magnetic field sensitivity of 1.9 nm/mT, the temperature sensitivities was measured to be 1.56 nm/°C [23]. For the tapered LPFGs, the two resonant wavelengths exhibit responsive differences in magnetic

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field and temperature [24]. However, most LPFGs-based MFSs are easily affected by temperature. Therefore, it is important to eliminate temperature interference for LPFGs-based MFSs. A cascaded fiber structure comprising MF-infiltrated micro-tapered LPFGs and FBG can solve the cross-sensitivity for temperature [25]. In our previous work, a novel fiber sensor based on arc-induced LPFGs in capillary (CLPFGs) has been demonstrated, with advantages of low cost and good flexibility. Moreover, CLPFGs present temperature insensitive behaviors [26].

In this paper, we present a magnetic field sensing by MF-coated CLPFGs. The arc-discharged CLPFGs were immersed with MF and then packaged in a glass tube. Experimental discussion is done on how the suggested sensor responds to the strength of external magnetic field. When magnetic field intensity changes, the intensity of resonant dip changes accordingly. The CLPFGs with different grating lengths of 8.5, 9 and 10 mm have been studied comparatively. When the grating length was 9 mm, the magnetic field sensitivity could achieve 0.036 dB/Oe. Moreover, the temperature disturbance has little influence on the MFS. The presented MF-coated CLPFGs provide potential application prospects in magnetic field sensing.

2. Methodology

2.1. Design and principle

Figure 1 displays the schematic representation of CLPFGs with MF coatings. MF is a type of unique nano intelligent material whose rheological characteristics are changed hinging upon the strength of applied magnetic field. Besides, MF has obvious magneto-optical effect. For MF, solid magnetic particles will group together when an external magnetic field is present. As the magnetic field intensity changes, the refractive index of the MF can be expressed as [25]:

$$n_{MF} = [n_s - n_b] \left[coth\left(\alpha \frac{H - H_{c,n}}{T}\right) - \frac{T}{\alpha \left(H - H_{c,n}\right)} \right] + n_b$$
(1)
for $H > H_{c,n}$

where $H_{c,n}$ is the critical magnetic field intensity depending on the type of carrier fluid and the volume concentration of nanoparticles, α corresponds to a fitting coefficient, and n_b and n_s are the initial and saturation values of n_{MF} , respectively.

The coupling mechanism of LPFGs is the coupling between forward transmitted core fundamental mode and forward transmitted cladding mode, when light propagates in the LPFGs, the periodic refractive index grating structure produces resonance attenuation in the spectrum [22]. In addition, the transmission minimum or resonance dip of the LPFGs is a function of the



coupling constant κ and the grating length *L* [27], which can be defined as:

$$T = \cos^2(\kappa L) \tag{2}$$

The coupling constant κ decreases with the increase of external disturbances such as ambient refractive index, bending, and lateral load. We use MF as the environmental medium and coat it on the outside of the grating structure. When applying external magnetic field, magnetohydrodynamic nanoparticles wrapped on the CLPFGs grating structure are magnetized, resulting in a magnetostrictive effect, which in turn causes the axial strain of the CLPFGs [28].

2.2. Fabrication and measurement setup

In the experiment, the CLPFGs have been fabricated using arc-discharged method as our previous work [26]. The Fe₃O₄ MF (EMG605 Ferro Tec) used in this experiment has a volume fraction of 3.6% of magnetic particles, and the diameter of magnetic particles suspended in base solution is about 10 nm. The refractive index of the MF is estimated to be around 1.40 without external magnetic field. When the intensity of the external magnetic field increases, particles gather in the direction of the magnetic field, forming columnar or chain-like structures in the liquid [27]. Figure 2(a) displays packing procedure of the sensor. First, we inserted the fabricated CLPFGs grating structure into a glass tube, which has an inner diameter of 1 mm, adjusted the position of the glass tube to ensure coverage of the grating area, and then fixed the sensor. Because of the viscosity of the MF material, we used a syringe with a needle tubing inner diameter of 0.1 mm to inject the MF from one end of the glass tube. Finally, for purpose of preventing the volatilization and leakage of the MF, ultraviolet (UV) glue is utilized to seal both ends of the glass tube, and the UV light is used to accelerate the solidification of the glue. Figure 2(b) shows the image of the packaged MF-coated CLPFGs. The total length of the packaged MF-coated CLPFGs is ~ 4 cm.

A magnetic field sensing system was created to look into the projected capabilities of CLPFGs for magnetic field sensing. Figure 3 displays the schematic diagram of experimental setup for measuring magnetic fields, which mainly include a broadband light source (BBS, SC-5, YSL), an optical spectrum analyzer (OSA, AQ6317B, ANDO), a tesla meter, a pair of electromagnets, and a current source. The MF-coated CLPFGs sensor is placed vertically between the magnetic poles of two electromagnets. The magnetic field strength created in region could be continually modified by modifying generating current, and to observe the magnetic field timely, the sensor of tesla meter can be placed as close as possible to the area to be measured. At room temperature, the light emitted by the BBS is transmitted to the grating area covered by a magnetic field and then connected to the OSA through an output SMF to obtain spectral performance.

3. Results and Analysis

The magnetic field sensing characteristics of MF-coated CLPFGs were tested at room temperature. At first, we measured the magnetic field sensing response of the bare CLPFGs with length of 8.5 mm, which has two resonant dips (dip A and dip B) at 1378.4 nm and 1483.8 nm, respectively, as shown in Figure 4(a). We measured the magnetic field sensing response of the sensor when it was not encapsulated by MF, with the magnetic field changing from 150 to 500 Oe, the resonant dip A







Figure 3 Schematic diagram of experimental setup for magnetic field sensing



and dip B exhibit magnetic field sensitivity of 0.0009 dB/Oe and -0.001 dB/Oe, respectively, as shown in the insertion of Figure 4(a). Before the packaging, the sensor was insensitive to magnetic fields. Figure 4(b) illustrated the spectra of CLPFGs with a grating length of 8.5 mm before and after MF packaged,

and it can be observed that there is a redshift in resonant wavelength and the transmissive intensity and the loss both ascend significantly. The wavelengths of dip A shift from 1378.4 nm to 1397.6 nm, respectively, totaling 19.2 nm, and the contrast changes 10.286 dB from -35.806 dB to -25.52 dB. And the wavelengths of dip B are shifted from 1483.8 nm to 1503.2 nm, respectively, and total is 19.4 nm; the contrast changes 2.311 dB from -41.42 dB to -39.109 dB. When the CLPFGs are wrapped in MF, the refractive index of external environment changes, which results in spectral characteristics of the CLPFGs.

The transmission spectra of CLPFGs with an 8.5 mm grating length shift when magnetic field intensity changes, as displayed in Figure 5(a). The two resonant dips can be seen to steadily develop as magnetic field strength increases. As the surrounding magnetic field increases from 150 to 500 Oe, the transmissive intensities of the dip A increased from -24.599 dB to -23.517 dB and dip B increased from -35.999 dB to -30.048 dB, respectively. The external magnetic field causes magnetization of Fe₃O₄ nanoparticles on the CLPFGs structure and the generated magnetostrictive strain leads to the strain optical effect of CLPFGs. And the structure of the CLPFGs is affected by magnetostrictive strain, the refractive index of entire grating region changes [28]. Figure 5(b) displays the relationship of transmissive intensity of two resonant dips on magnetic field

Figure 4 (a) Magnetic field characterization of the initial CLPFGs before packaged and (b) Transmission spectra of the magnetic field sensors before and after MF packaged



Figure 5 (a) Measured spectra with various magnetic field intensities of the 8.5-mm length CLPFGs MFS and (b) Relationship between the resonant dips and magnetic field intensity





variations. The magnetic field sensitivities of dip A and dip B obtained through linear fitting are 0.003 dB/Oe and 0.017 dB/Oe, respectively. When the resonant dip has larger transmissive depth, it presents faster descend to external magnetic field, resulting in higher sensitivity.

Due to the transmissive and coupling properties of initial CLPFGs [26], the grating length could influence the sensing behaviors, so the magnetic field sensing characteristics of CLPFGs with different lengths were further studied. Figure 6(a)displays the transmission spectrum response of MF-coated CLPFGs with grating length of 9 mm on the surrounding magnetic field increases. The coupling depth of dip A in 9-mm CLPFGs is greater than that of dip B. It has different coupling efficiency with the resonant inclination angle of 8.5 mm CLPFGs. And the dip B is around 1600 nm, which has higher order cladding mode and has a higher sensitivity [26]. Figure 6(b) illustrates the relationship between the resonant dips and magnetic field intensity, which exhibits the similar magnetic field sensing characteristics as 8.5-mm length CLPFGs. As the surrounding magnetic field rises from 150 to 500 Oe, the transmissive intensities of dip A and dip B increased. However, when the magnetic field intensity exceeds 220 Oe, the magnetic fluid reaches a saturation state, and the magnetostrictive effect decreases leading to the gradual decrease in transmission loss changes. As shown in Figure 6(c), we record every minute until the spectrum remains stable, and the average response time of the sensor is approximately 5 minutes.

Figure 7(a) displays the transmission spectrum of CLPFGs at different magnetic field intensities when grating length is 10 mm. Two resonant dips have been detected at 1552.4 nm (dip A) and 1618.1 nm (dip B), with corresponding contrasts of -29.30 dB and -41.95 dB. As the intensity increases, the resonant wavelength shifts slightly, and the transmissive intensity shows a slow increasing trend. When magnetic field rises from 150 Oe to 500 Oe, the contrast changes are $-29.302 \sim -25.543$ dB and $-41.945 \sim -29.49$ dB, respectively. According to Figure 7(b), linear fitting shows that magnetic

field sensitivities of dip A and dip B are 0.012 dB/Oe and 0.034 dB/Oe, respectively.

Table 1 shows magnetic field sensitivity of MF-coated CLPFGs with different gratings lengths. LPFGs can perceive changes in optical properties caused by magnetic fields, and their transmission minimum and resonant wavelength are extremely sensitive to changes in surrounding medium. By introducing LPFGs into capillary fibers, the coupling between propagation core mode and cladding mode is promoted. And we can observe that the resonant dip presents faster descend to external magnetic field as larger transmissive depth achieved, which results in higher sensitivity. When the length of the capillary fiber grating is 9 mm,

 Table 1

 Sensitivity comparison of the MFSs with different capillary long-period grating structures

	Magnetic field sensitivity (dB/Oe)		Magnetic field range (Oe)
	Dip A	Dip B	
8.5-mm CLPFGs	0.003	0.017	150~500
9-mm CLPFGs	0.028	0.036	150~500
10-mm CLPFGs	0.012	0.034	150~500

the CLPFGs sensor achieves a maximum magnetic field sensitivity of 0.036 dB/Oe.

In addition, the temperature characteristics of the sensor are measured experimentally, as shown in Figure 8. The contrasts of MF-coated CLPFGs sensor do not change significantly with temperature varies. Therefore, the sensor is insensitive to temperature. The temperature cross sensitivity may be disregarded due to the low temperature sensitivity. Compared with other grating-based MFSs, the suggested MF-coated CLPFGs-based MFS could be used to accurately detect the magnetic field strength.

Figure 6 (a) Measured spectra with various magnetic field intensities of the 9-mm length CLPFGs MFS, (b) Relationship between the resonant dips and magnetic field intensity, and (c) Determination of the response time of the CLPFGs



Figure 7

(a) Measured spectra with various magnetic field intensities of the 10-mm length CLPFGs MFS and (b) Relationship between the resonant dips and magnetic field intensity



Figure 8 Contrasts variation with the increase of temperature



4. Conclusion

In conclusion, we presented a temperature-insensitive MF-coated CLPFGs MFS. The CLPFGs were fabricated by arc discharge method and then immersed with the MF. The magnetic field sensing characteristics of bare and MF-coated CLPFGs have been investigated experimentally. With MF coating, the magnetic field sensing sensitivity could be enhanced. The experimental results demonstrate that with the increasing external magnetic field, the intensity of resonant dips gradually decreased, which is caused by magnetostrictive effect together with refractive index variations. Moreover, the magnetic field sensing characteristics of CLPFGs with grating lengths of 8.5, 9 and 10 mm were studied comparatively. When the grating length of the CLPFGs is 9 mm, the sensor can realize a sensitivity of 0.036 dB/Oe. In addition, the presented sensor can measure the magnetic field without temperature cross-sensitivity. The proposed sensor has the advantages of simple structure, low cost, and convenient to fabrication performance and exhibits promising application prospects.

Recommendations

The magnetic field sensing research based on MF materials and CLPFGs studied in this article is conducted under the condition that the electric field direction of the incident light is perpendicular to the emission direction of the magnetic field. If it is necessary to study the characteristics of magnetic field changes under parallel or other angles, further research is needed.

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Ethical Statement

This study does not contain any studies with human or animal subjects performed by any of the authors.

Conflicts of Interest

Yunhe Zhao is an Associate Editor for Journal of Optics and Photonics Research, and was not involved in the editorial review or the decision to publish this article. The authors declare that they have no conflicts of interest to this work.

Data Availability Statement

Data are available from the corresponding author upon reasonable request.

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